

# THE UNITED STATES OF AMERICA

TO ALL TO WHOM THESE PRESENTS SHALL COME:

UNITED STATES DEPARTMENT OF COMMERCE  
United States Patent and Trademark Office

August 04, 2004

THIS IS TO CERTIFY THAT ANNEXED HERETO IS A TRUE COPY FROM  
THE RECORDS OF THE UNITED STATES PATENT AND TRADEMARK  
OFFICE OF THOSE PAPERS OF THE BELOW IDENTIFIED PATENT  
APPLICATION THAT MET THE REQUIREMENTS TO BE GRANTED A  
FILING DATE.

APPLICATION NUMBER: 60/480,453

FILING DATE: June 20, 2003

RELATED PCT APPLICATION NUMBER: PCT/US04/19587

RECEIVED

09 AUG 2004

WIPO PCT

By Authority of the  
COMMISSIONER OF PATENTS AND TRADEMARKS



M. SIAS  
Certifying Officer



**PRIORITY  
DOCUMENT**  
SUBMITTED OR TRANSMITTED IN  
COMPLIANCE WITH RULE 17.1(a) OR (b)

Under the Paperwork Reduction Act of 1995, no persons are required to respond to a collection of information unless it displays a valid OMB control number.

**PROVISIONAL APPLICATION FOR PATENT COVER SHEET**

This is a request for filing a PROVISIONAL APPLICATION FOR PATENT under 37 CFR 1.53(c).

Express Mail Label No.

EV325929951US

U.S. PTO  
480453  
17537  
06/20/03**INVENTOR(S)**

Given Name (first and middle [if any])  LOUIS WILLIAM DAVID JAMES	Family Name or Surname  LHERBIER NOVOTNAK	Residence (City and either State or Foreign Country)  Pittsburgh, Pennsylvania McDonald, Pennsylvania
--	--	---

 Additional inventors are being named on the \_\_\_\_\_ separately numbered sheets attached hereto**TITLE OF THE INVENTION (500 characters max)****MANUFACTURING OF CONTROLLED POROSITY METALLIC TOOLS**

Direct all correspondence to:

 Customer Number**CORRESPONDENCE ADDRESS**

000110

Place Customer Number  
Bar Code Label here

OR

Type Customer Number here

 Firm or  
Individual Name

DANN, DORFMAN, HERRELL AND SKILLMAN, P.C.

Address

1601 Market Street

Address

Suite 2400

City

Philadelphia

State

PA

ZIP

19103-2307

Country

US

Telephone 215-563-4100

Fax 215-563-4044

**ENCLOSED APPLICATION PARTS (check all that apply)** Specification Number of Pages

6

 CD(s), Number Drawing(s) Number of Sheets

1

 Other (specify)

Claims: 1 page

 Application Data Sheet. See 37 CFR 1.76**METHOD OF PAYMENT OF FILING FEES FOR THIS PROVISIONAL APPLICATION FOR PATENT** Applicant claims small entity status. See 37 CFR 1.27.**FILING FEE  
AMOUNT (\$)** A check or money order is enclosed to cover the filing fees

04-1406

\$160.00

 The Commissioner is hereby authorized to charge filing fees or credit any overpayment to Deposit Account Number: Payment by credit card. Form PTO-2038 is attached.

The invention was made by an agency of the United States Government or under a contract with an agency of the United States Government.

 No. Yes, the name of the U.S. Government agency and the Government contract number are: \_\_\_\_\_

Respectfully submitted,

SIGNATURE

Vincent T. Pace

TYPED or PRINTED NAME

Vincent T. Pace

TELEPHONE

215-563-4100

Date 06/20/2003

REGISTRATION NO.  
(if appropriate)  
Docket Number:

31,049

0008-CA323PRO

**USE ONLY FOR FILING A PROVISIONAL APPLICATION FOR PATENT**

This collection of information is required by 37 CFR 1.51. The information is used by the public to file (and by the PTO to process) a provisional application. Confidentiality is governed by 35 U.S.C. 122 and 37 CFR 1.14. This collection is estimated to take 8 hours to complete, including gathering, preparing, and submitting the complete provisional application to the PTO. Time will vary depending upon the individual case. Any comments on the amount of time you require to complete this form and/or suggestions for reducing this burden, should be sent to the Chief Information Officer, U.S. Patent and Trademark Office, U.S. Department of Commerce, Washington, D.C. 20231. DO NOT SEND FEES OR COMPLETED FORMS TO THIS ADDRESS. SEND TO: Box Provisional Application, Assistant Commissioner for Patents, Washington, D.C. 20231.

## MANUFACTURING OF CONTROLLED POROSITY METALLIC TOOLS

Louis William Lherbier  
David James Novotnak

### Background of the Invention

Plastic injection molding is a very large industry, and we rely on hundreds of plastic injection molded products every day. The list is endless, but includes interior automotive parts, cell phone cases and windows, caps and closures, children's toys, kitchen items, office equipment, etc. Even though great advances have been made in this industry, product complexity and production rates are still limited. These limitations do not result from the injection molding machines themselves, but rather from the restrictions imposed by tooling design and tooling materials used in the injection molding machines.

The known tools for injection molding machines are made from cast and wrought steel and have been available for over 50 years. The known injection molding tools exhibit a number of disadvantages. The known machines are designed so that air can vent from the mold cavity as it is filled with the plastic material. The tools are usually inefficiently cooled by water passing through channels drilled into the mold walls. Production efficiency is low because the plastic component must remain in the mold until it is solid enough to hold its shape and be ejected. Other features such as surface quality can also be impaired by cooling inefficiencies. Better and more consistent cooling of the mold would mean that the plastic solidifying temperature could be reached sooner, thus reducing cycle time, and increasing productivity.

Based on current knowledge of gas and gas usage, polymer processing techniques, and the metallurgy of tool materials, a new cooling technology has been developed which has been described as a major breakthrough for the plastic forming

industry and especially for plastic injection molding. This technology holds promise for increased productivity, greater design freedom for complex products, increased profits and a widened product scope because it has the potential to reduce production cycle times by 20 to 40%.

The new technology is an advanced cooling concept in which liquid cooling gas is injected into the mold where it evaporates. The resulting gas vents from the mold. This technology requires a mold material manufactured with uniform and controlled porosity to effect optimum cooling. By using micro pores in the mold material, the evaporative cooling points can be situated close to the forming surface of the mold. There is no restriction on the geometry of the mold in the same way as molds made with drilled water channels.

While the technology of gas cooling is viable, the difficulty has been the availability of a suitable material for the molds and the inability to obtain a controlled and consistent quality level of microporosity in the mold material. Further, no efficient technique was available to manufacture a composite mold with a porous interior and a solid surface layer, as is required in many applications where surface quality is of paramount importance.

Attempts to manufacture such tooling by conventional powder metallurgy press-and-sinter techniques have failed to produce the desired results. Those techniques cannot produce the required porosity levels with the degree of control required. Moreover, the press-and-sinter technique produces a non-uniform pore size in the tool material. With this type of variation, the cooling of the tool surface cannot be controlled, and the positives of the new gas cooling technique cannot be effectively utilized. Further, conventional powder metallurgy press and sinter technology cannot produce a solid surface on the tool, while at the same time producing a controlled and consistent microporous substructure.

It is clear that a material and process needs to be developed to manufacture tooling that can take advantage of the new gas cooling concept for plastic injection molding tools and molds. The process according to the present invention involves the utilization of corrosion resistant materials in combination with a powder metallurgy consolidation process that can produce a microporous tool with controlled porosity and pore size. Further, the consolidation technology according to this invention can produce composite tools designed to have both solid surfaces and porous areas as required for a particular application. Unlike other powder metallurgy consolidation processes, the process according to the present invention provides higher pressure, lower consolidation temperatures, and lower cycle times by orders of magnitude. These advantages result in lower manufacturing costs and significantly lower capital investment.

This new process of manufacturing controlled and uniformly consistent microporous corrosion resistant tool products will not only increase plastic injection molding productivity by 20 to 40%, but also eliminate many inherent cooling and quality difficulties common with conventional mold technology. Because the molds are porous, air can vent through the walls of the mold as the plastic material is being injected. This eliminates the venting problem of conventional molds. In addition, after injection of the plastic into the mold cavity, a small amount of liquid gas can be injected into the mold to release the part quickly and easily. The result will be fewer jammed injection machines, and fewer rejects for ejector marks. Overall, this technology provides tooling for plastic injection molding that has part cooling, air venting, and surface quality advantages over tooling currently used in the industry.

#### Detailed Description

The present invention includes a process for manufacturing a corrosion resistant, microporous material product with open and/or closed surfaces that can be used to effect uniform and consistent cooling of tools used for plastic injection

molding. The process initially involves producing gas atomized powder metals by known powder metallurgy techniques. In a second step, a shaped container is prepared for holding the powdered metal. The powder-filled container is heated to an appropriate temperature and then consolidated. The assembly is consolidated quasi-isostatically in a liquid medium at controlled pressure by means of a standard hydraulic press. The consolidation process is essentially a one-step operation.

A preferred embodiment of the process according to the present invention will now be described with reference to Figure 1 of the drawings. The material for the microporous tool is selected in accordance with the operating environment of the plastic injection molding process and the components to be manufactured. The gas atomized metal powder is screened to a particle size distribution consistent with the porosity level, pore size, and strength required by the mold application. Powder particle size is not a critical variable. Therefore, a wide range of powder particle sizes can be used for cost effectiveness. Good results have been obtained with powder particle sizes of -80 mesh and smaller. However, it will be appreciated that different sizes may be more appropriate for other types of injection molding tools. The screened powder is vibration filled into a shaped container. The shape of the container is dictated by the physical design of the injection mold. The powder-filled container is evacuated, sealed by crimping the evacuation nozzle, and then welded shut.

Consolidation of the metal powder proceeds as follows. The powder/container assembly is placed in an open metal vessel in which it is surrounded by glass frit. The metal vessel containing the powder/container assembly and the glass frit is placed into a furnace. The metal vessel is heated to a temperature appropriate for the tool material and high enough to melt and liquify the glass frit. After an appropriate time to reach temperature uniformity, the vessel/container assembly is removed from the furnace. It is placed in a pot die that is placed or located in a hydraulic press. Sufficient pressure is applied with the press to the assembly in the pot die to consolidate the metal powder

while retaining the desired amount of porosity. The pressure transfer medium in the pot die is a molten but highly viscous glass frit. After pressing, the consolidated powder and container assembly is ejected from the press and allowed to cool to room temperature. Figure 2 (upper) shows a fully porous tool blank made by the process according to the present invention.

Consolidation trials on alloys 420 LC and H13 have demonstrated that porosity can be controlled from a low of 60% dense to 100% dense. Pore size can also be controlled by process variables. Key variables of the process include powder particle size, consolidation temperature, and the pressure exerted by the hydraulic press. A preferred temperatures range is about 1850°F

to about 2050°F. A preferred forging pressure range is about 250 tons to about 600 tons. The liquid glass media exerts a quasi-isostatic pressure on the containerized metal powder and produces a substantially uniform porosity throughout the entire product. Additionally, the relatively low pressing temperatures help prevent the formation of deleterious phases in the matrix material that may form in complex alloys at the higher temperatures used in the conventional powder metallurgy consolidation processes.

Surface finish is critical for some injection molded plastic parts and a fully porous tool would not provide the desired surface finish. To resolve that problem, composite tools with areas of solid and porous structure, as well as composite tools with varying material compositions, can also be produced by a process according to another aspect of the present invention. The alternate procedure includes the placement of a piece of a solid, cast and wrought, material in the metal container prior to filling in the metal powder. The metal container is then filled with the metallic powder and consolidated as described above. The metal powder bonds to the solid material during the consolidation step. The resulting tool product has a composite structure consisting of a fully dense surface layer and an internal porous substructure. Figure 2 (lower) shows a composite tool blank made by the process according to this invention. This

composite structure provides a tool that has a good surface for interfacing with the plastic part while still providing the desired cooling effect afforded by the porous substructure.

In view of the foregoing description, some of the novel features and advantages of the process according to the present invention should now be apparent. The process according to this invention can produce controlled porosity levels in plastic injection molding tools more uniformly and at lower costs than the known powder metallurgy consolidation techniques. Both large and small tools with uniform porosity can be produced by the process. The use of this process to manufacture tools for plastic injection molding will have a significant positive economic impact on this very important industry.

WHAT IS CLAIMED IS:

1. A process for making a metal tool having controlled porosity, comprising the steps of:

- (a) preparing metal powder by gas atomization;
- (b) filling a metal container with the metal powder;
- (c) placing the powder-filled container in a metal vessel;
- (d) surrounding the powder-filled container in the metal vessel with glass frit;
- (e) heating the metal vessel to temperature sufficient to melt the glass frit; and then
- (f) compacting the metal vessel under sufficient pressure to partially consolidate the metal powder so as to retain a desired amount of porosity therein.

2. A process for making a composite metal tool having controlled porosity, comprising the steps of:

- (a) preparing metal powder by gas atomization;
- (b) placing a piece of a fully consolidated metal in a metal container;
- (c) filling the metal container with the metal powder;
- (d) placing the powder-filled container in a metal vessel;
- (e) surrounding the powder-filled container in the metal vessel with glass frit;
- (f) heating the metal vessel to temperature sufficient to melt the glass frit; and then
- (g) compacting the metal vessel under sufficient pressure to bond the metal powder to the fully consolidated metal piece and to partially consolidate the metal powder so as to retain a desired amount of porosity therein.

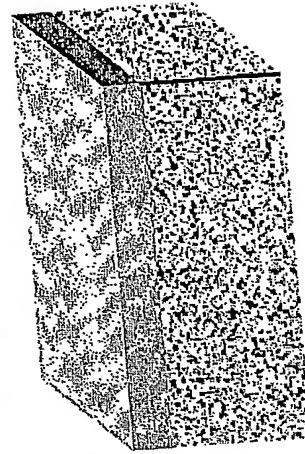
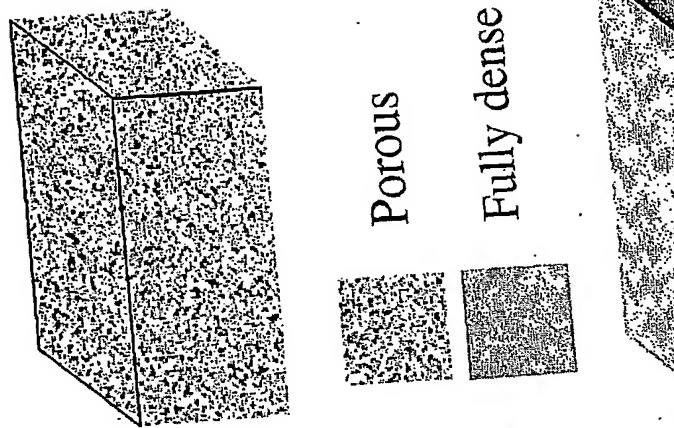


Figure 2 Resultant tool blank as porous or combination porous-fully dense

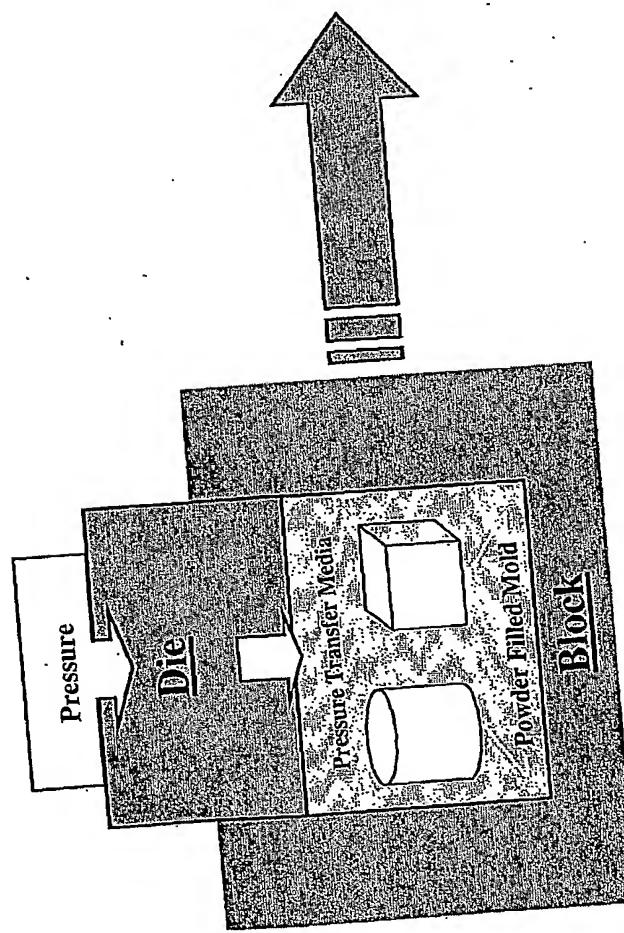


Figure 1 Quasi isostatic compaction of shaped containers